Table VII. Empirical Constants a and b for the Ternary System Correlation





Figure 13. Empirical constant "b" is a function of internal pressure difference between solvent and 2,4-DMP

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Heat Content of Platinum

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CHEMICAL INERTNESS, high melting point, and freedom from allotropic and magnetic transformations give platinum obvious advantages as a secondary standard for calibrating high-temperature calorimeters. However, currently accepted tables (8, 13) of the heat content of platinum can be criticized because the values below 500° K. are too high to join smoothly with reliable low-temperature $(<298^{\circ}$ K.) heat capacity data (1, 12), and because the tables are based mainly on the drop calorimetry of Jaeger and others (4, 5, 6) in which, as Oriani (10) has pointed out, the heat lost by the sample during the drop was not properly taken into account.

The performance of a diphenyl ether calorimeter used in this laboratory is routinely checked by dropping samples of platinum. The results so obtained scatter considerably more than those by Jaeger and others (4, 5, 6) from larger samples, but they do show clearly that the over-all systematic error in Jaeger's work is very small. They also show the previously tabulated heat contents at 400° and 500° K. are somewhat too high.

EXPERIMENTAL

Since the diphenyl ether calorimeter has been described previously (3), the procedure and sample preparation will be described here only briefly.

Four samples, each about 99.99% pure, were used in the determinations. The first was a solid sphere about 8 mm. in diameter weighing 5.6 grams. The second was formed from 0.7 gram of 0.127 mm. platinum foil to make a hollow sphere of the same diameter as the first. The third and fourth samples were similar to the second, except that they were filled with 1.9 grams of platinum wire and 1.1 grams of platinum foil, respectively.

The samples were heated under an argon atmosphere in a resistance furnace to a measured temperature, T, then dropped into the diphenyl ether calorimeter. The heat liberated by a sample within the calorimeter is absorbed by a mixture of liquid plus solid diphenyl ether, melting some of the solid without changing its temperature. The expansion accompanying melting forces mercury from a pool in the bottom of the diphenyl ether chamber out into a calibrated horizontal capillary tube. The heat given up by the sample within the calorimeter can be found by multiplying the weight of mercury displaced by the factor 18.91 cal./gram Hg determined by Jessup (7) at the National Bureau of Standards. To obtain the heat content of the sample at temperature T, one must add a quantity δ representing the heat lost during the drop from furnace to calorimeter. If q_1 and q_2 correspond to the heat effects observed when two samples containing m_1 and m_2 g-atoms of platinum are dropped from the same initial temperature, T, then the heat content per gram atom relative to 300° K., the melting point of diphenyl ether, will be

$$H_T - H_{300} = \frac{q_1 + \delta_1}{m_1} = \frac{q_2 + \delta_2}{m_2}$$

For samples of the same size, shape, and emissivity, $\delta_1 = \delta_2$, so that δ can be determined by measurement of the heat and mass of two of the four samples described. An analysis of many measurements has yielded a set of δ -values (Figure 1) which is consistent with the results from all four samples. The experimental results referred to 298.15° K. are given in Table I and plotted in terms of the function $(H_T^0 - H_{298.15}^0)/(T - 298.15)$ in Figure 2 with the results of Jaeger and others (4, 5, 6) and White (14). The scatter of present results ($\pm 0.5\%$) is greater than that of the more precise measurements of Jaeger and others ($\pm 0.1\%$) and White



Table I. Experimental Results

<i>T</i> . ° K.	$H_{T}^{0} - H_{29815}^{0},$ Cal./G. Atom	<i>T</i> . ° K.	$H_T^0 - H_{298.15}^0$, Cal./G. Atom	<i>T</i> .°K.	$H_T^0 - H_{296.15}^0$, Cal./G. Atom	T, ° K.	$H_T^0 - H_{298,15}^0$, Cal./G. Atom
-,	(Platinum S	Sphere)		-,	(Platinum W	ire Sample)	
339.1 343.8 344.5 344.6 345.8 346.3 346.5 351.5 351.8 358.6 366.8 380.5 384.8 386.7 388.4 396.7 397.1	253 282 286 296 299 331 334 375 429 514 537 533 560 615 614	600.5 658.6 658.6 675.0 682.0 687.4 688.4 701.8 705.3 717.1 782.3 797.3 799.9 803.9 804.0 822.4 832 1	$1933 \\ 2319 \\ 2322 \\ 2426 \\ 2468 \\ 2504 \\ 2507 \\ 2598 \\ 2629 \\ 2704 \\ 3155 \\ 3259 \\ 3263 \\ 3276 \\ 3304 \\ 3415 \\ 3462 \\ 3462 \\ 3462 \\ 3319 \\ 3462 \\ 3319 \\ 3415 \\ 3462 \\ 3462 \\ 3415 \\ 3462 \\ 3462 \\ 3415 \\ 3462 \\ 3462 \\ 3415 \\ 3462 \\ 3462 \\ 3415 \\ 3462 \\ 3462 \\ 3415 \\ 3462 \\ 3462 \\ 3415 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ 3462 \\ $	500.5 512.4 518.9 520.1 596.1 597.8 599.5 602.9 620.2 631.9 633.1 638.3 682.3 688.0 698.0 719.0 794.7	1277 1366 1389 1400 1900 1908 1923 1937 2070 2123 2129 2166 2473 2511 2589 2722 3237	910.7 989.5 989.5 991.3 998.0 1001.3 1005.7 1035.0 1101.8 1105.8 1107.5 1163.5 1174.9 1186.2 1191.0 1192.1 1202.0	$\begin{array}{r} 4039\\ 4575\\ 4603\\ 4566\\ 4656\\ 4649\\ 4701\\ 4888\\ 5399\\ 5451\\ 5431\\ 5863\\ 5925\\ 6012\\ 6023\\ 6017\\ 6134\end{array}$
397.1 400.3 400.6 400.8 403.8 403.9 405.5 415.4 448.7 452.6 457.6 453.0	614 636 642 639 656 659 671 731 940 973 994 1157	832.1 861.2 875.0 878.0 894.9 895.3 895.4 902.7 907.0 909.7 909.7 949.2 961.8	3462 3681 3784 3801 3923 3924 3923 3963 3986 4012 4294 4377	794.7 796.7 798.5 819.6 826.7 888.5 888.6 892.7 894.2 895.7	3237 3257 3263 3425 3422 3894 3886 3912 3921 3936 (Platinum F	1202.0 1208.5 1291.7 1297.8 1298.0 1395.2 1397.3 1428.6 1434.5 1436.0 oil Sample)	6134 6165 6765 6819 6807 7508 7623 7791 7836 7839
$\begin{array}{r} 483.9\\ 483.8\\ 487.2\\ 490.1\\ 492.3\\ 494.7\\ 496.6\\ 499.7\\ 503.8\\ 505.3\\ 505.6\\ 576.8\\ 577.0\\ 586.9\\ 593.1\\ 593.6\\ 595.9\\ 598.1\\ \end{array}$	$1164 \\ 1175 \\ 1186 \\ 1191 \\ 1213 \\ 1222 \\ 1230 \\ 1253 \\ 1275 \\ 1301 \\ 1312 \\ 1315 \\ 1767 \\ 1776 \\ 1848 \\ 1884 \\ 1889 \\ 1903 \\ 1913 \\ 1913$	973.3 981.6 988.5 989.3 990.2 997.3 1026.4 1030.5 1063.8 1106.0 1113.9 1208.0 1294.1 1295.5 1296.6 1389.0 1391.2 1403.8	$\begin{array}{c} 4466\\ 4526\\ 4572\\ 4581\\ 4586\\ 4619\\ 4859\\ 4869\\ 5107\\ 5419\\ 5500\\ 6143\\ 6828\\ 6775\\ 6794\\ 7553\\ 7512\\ 7634 \end{array}$	503.0 584.2 669.5 691.2 757.5 797.4 804.7 879.2 894.2 897.9 905.1 905.6 949.5 989.9 997.5 999.1 1020.6 1022.6 1045.2 1071.8 878.8	$\begin{array}{c} 1301\\ 1840\\ 2394\\ 2537\\ 2981\\ 3261\\ 3293\\ 3832\\ 3938\\ 3967\\ 3979\\ 3967\\ 4325\\ 4573\\ 4629\\ 4627\\ 4819\\ 4812\\ 5002\\ 5150\\ 5228\\ \end{array}$	$1093.1 \\ 1093.5 \\ 1094.0 \\ 1095.3 \\ 1160.4 \\ 1189.3 \\ 1193.7 \\ 1194.4 \\ 1198.6 \\ 1209.5 \\ 1284.4 \\ 1296.0 \\ 1296.3 \\ 1300.5 \\ 1306.0 \\ 1375.9 \\ 1377.8 \\ 1380.2 \\ 1382.0 \\ 1393.7 \\ 1400.7 \\ 1400.7 \\ 1400.7 \\ 1095.3 \\ 1095.3 \\ 1095.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1005.3 \\ 1$	5356 5372 5333 5380 5815 6039 6075 6066 6123 6195 6752 6826 6772 6874 6866 7405 7375 7440 7434 7472 7548

 $(\pm 0.3\%)$. They therefore contribute nothing to the precision of the values. They do show, however, that there is no important systematic error in the work of Jaeger and others such as would occur from significant uncompensated losses of heat during the drop of the samples. They also show that the tabulated values of Kelley (8) and Stull and Sinke (13) at 400° and 500° K, are too high and thus make reasonable a choice of new values at these temperatures which agree with low temperature C_{ν} data (1, 12). C_p is molal heat capacity at constant pressure.



Figure 2. Heat content of platinum expressed in terms of the function $(H_T - H_{298,15})/T - 298.15)$

DISCUSSION

The three sets of heat content measurements (Figure 2) can be fitted within 0.2% by the analytical expression

$$H_T^0 - H_{298,15}^0 = 0.0006425 T^2 + 5.796 T - 1785$$

which is shown as a solid line. Although the data are somewhat more closely fitted by the two equations (Figure 2) which Jaeger and others (4, 5, 6) use to describe their results, the scatter in existing data would not seem to warrant such a refined description. The thermodynamic properties of platinum given in Table II have been calculated from the above equation and are considered to be accurate within 0.3%. Measurements reported prior to 1918 seemed too unreliable to warrant any weight in the final selection. The heat content data of Esser, Averdieck, and Grass (2) were rejected because their sample was contaminated with iridium. C_p measurements of Persoz (11) on a sample of unstated purity were also rejected as being too low.

It is encouraging that the new selection joins smoothly in both C_p and (dC_p/dT) with the extrapolated lowtemperature measurements of Simon and Zeidler (12) and Clusius, Losa, and Franzosini (1). The values given in Table II are thought to be both more reliable and more self-consistent than those of previous tabulations (8, 13). Values of the free energy function are based on $S_{298.15}^0 =$ 9.95 ± 0.05 as given by Kelley and King (9).

Table II. Thermodynamic Values for Platinum

			Cal./Deg. G. Atom		
	$H^0_T - H^{-0}_{29815}$			$-(F_7^0 - H_{296.15}^0)$	
$T, \circ K$	Cal./G. Atom	C_{P}	$S_{\it T}^{\scriptscriptstyle 0}$ – $S_{\it 298.15}^{\scriptscriptstyle 0}$	T	
298.15	0	6.18	0.00	9.95	
300	11	6.18	0.04	9.95	
400	636	6.31	1.83	10.19	
500	1275	6.44	3.26	10.66	
600	1925	6.57	4.44	11.18	
700	2590	6.70	5.46	11.72	
800	3260	6.82	6.37	12.24	
900	3950	6.95	7.18	12.74	
1000	4650	7.08	7.92	13.21	
1100	5370	7.21	8.60	13.67	
1200	6100	7.34	9.23	14.10	
1300	6840	7.47	9.82	14.51	
1400	7590	7.60	10.38	14.91	
1500	8350	7.72	10.91	15.29	
1600	9130	7.85	11.41	15.65	
1700	9920	7.98	11.89	16.00	
1800	10730	8.11	12.35	16.34	
1900	11550	8.24	12.79	16.66	
2000	12380	8.37	13.22	16.98	
2043	12740	8.42	13.40	17.11	

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